

Prognosis Modeling of Nitrous Oxide Emissions after Catalytic Reduction

Maya Stefanova, Rozalina Chuturkova, Evgeni Sokolovski, Nina Ilieva, Tsenislav Vlaknenski

Abstract – The present research aims to assess the effect of increasing the thickness of a secondary catalyst layer for N_2O emission reduction at a nitric acid plant in Devnya, Bulgaria upon the ambient air quality. A mathematical modeling is done for simulating the dispersion of N_2O emissions from the plant into the ground atmospheric layer taking into account the specific topographic and meteorological conditions of the region. Separate graphic models are done illustrating the dispersion of N_2O emissions at two main scenarios – at current thickness of the secondary catalyst layer of 60 mm and at future increase of the catalyst layer thickness to 90 mm. Modeling results indicate that under equivalent meteorological conditions the planned increase of the secondary catalyst layer thickness leads to 69 % reduction of the annual average N_2O concentration in the atmosphere. Maximum N_2O concentrations over specific periods of time (1 hour, 8 hours and 24 hours) are also reduced over 3 times within the outlines of the exposed areas. Research results provide prognosis on the impact of the increased thickness of the secondary catalyst layer as a measure for N_2O emission reduction upon the ambient air quality of the source region. Prognosis modeling provides a tool for assessing the contribution of N_2O emissions from nitric acid production to the overall greenhouse gas emissions in long-term future periods regarding the implementation of quantitative commitments under the Kyoto Protocol.

Index Terms - ambient air quality, greenhouse gas emissions, nitrous oxide, prognosis air dispersion modeling, secondary catalyst layer.

I. INTRODUCTION

Nitric acid production is a major industrial source of nitrous oxide N_2O emissions, which is a greenhouse gas under the Kyoto Protocol and one of the main reasons for global warming effect [1]-[4]. There are 4 groups of measures developed for N_2O emission reduction at nitric acid production [5]-[9]. Primary measures are measures that affect the formation of N_2O during the catalytic oxidization of ammonia like modifying the geometry of the platinum gauze

which can lead to a higher conversion of ammonia to nitric oxide NO and/or a reduction in the formation of N_2O . Secondary measures are taken with regard to the process gas stream, produced in the process from the oxidisation catalyst, to the absorption tower (homogeneous decomposition, high temperature catalytic decomposition). Tertiary measures can be taken in the process that takes place between the absorption tower and the expansion turbine (low temperature catalytic decomposition, selective catalytic reduction with hydrocarbons, non-selective catalytic reduction of NOx with simultaneous N_2O reduction). Sequential (end-of-pipe) techniques are some of the techniques described as tertiary measures but placed behind the expansion turbine (selective catalytic reduction, catalytic decomposition). The implementation of a secondary non-platinum catalyst that decomposes N_2O to nitrogen and oxygen right after its formation in the reactor chamber is a secondary measure for catalytic N_2O emission reduction [10]-[24]. The efficiency of the reduction depends on multiple factors, most importantly on the specific technological conditions of the production process, the duration of the functional activity of the secondary decomposing catalyst and the thickness of the secondary catalyst layer [25]-[26]. Previous research indicates that catalytic reduction of N_2O emissions from nitric acid production affects positively the ambient air quality of the source region [27]-[28]. The present research's aim is to determine the prognosis level of additional N_2O emission reduction due to future increase of the secondary catalyst layer thickness at a nitric acid plant and its effect upon the ambient air quality taking into account the specific topography and meteorological conditions of the source region.

II. MATERIAL AND METHODS

Within the present research data on N_2O emissions from a single point source is used – an industrial plant for nitric acid production with capacity 363000 tons per year, situated in the industrial area of Devnya, Bulgaria. A secondary decomposing catalyst for N_2O emission reduction is implemented at the plant in September 2005 [29]. The catalyst layer is equally disturbed directly on top of the support grid of each reactor separated on top and bottom by steel screens. The thickness of the catalytic layer in the basket is approximately 28 mm. In August 2012 a reconstruction of the ammonia burning reactors is done in order to mount a deeper catalyst basket that increases the catalyst layer thickness to 60 mm [26].

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* Correspondence Author

Maya Stefanova*, Department of Ecology and Environmental Protection, Technical University, Varna, Bulgaria.

Assoc. Prof. Rozalina Chuturkova, PhD, Department of Ecology and Environmental Protection, Technical University, Varna, Bulgaria.

Evgeni Sokolovski, PhD, Department of Engineering Ecology, University of Chemical Technology and Metallurgy, Sofia, Bulgaria.

Nina Ilieva, PhD, Department of Engineering Ecology, University of Chemical Technology and Metallurgy, Sofia, Bulgaria.

Tsenislav Vlaknenski, Department of Ecology and Environmental Protection, Technical University, Varna, Bulgaria.

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A mathematical modeling is done that simulates the dispersion of N_2O emissions from the plant. Due to the fact that N_2O is inert in the troposphere, all models simulating emission dispersion from area, transport or point sources at urban areas are not applicable [30]-[39]. A practically approved software product BREEZE AERMOD is used within this research for N_2O emission dispersion modeling, taking into account the topography of the region.

In order to ensure maximum reliability of the meteorological conditions of the region validated data is used in the form of hourly meteorological file containing information on 6 parameters – wind speed and direction, ambient air temperature, relative humidity, atmospheric pressure, sun radiation intensity.

In order to avoid obtaining of wrong results due to variation of the meteorological conditions N_2O emission dispersion modeling is done over two main scenarios. The first scenario simulates the dispersion of N_2O emissions from the nitric acid plant at current thickness of the secondary catalyst layer of 60 mm, and the second scenario simulates the prognosis dispersion of N_2O emissions at future increase of the catalyst layer thickness up to 90 mm. The dispersion of N_2O emissions at 60 mm thickness of the secondary catalyst layer is simulated using emission data in the form of hourly N_2O concentration file for 2013 and meteorological data for the same year. The dispersion of N_2O emissions at planned increase of the thickness of the secondary catalyst layer up to

90 mm is simulated using prognosis data file on the reduced hourly N_2O concentration [26] and meteorological data for 2013 in order to provide comparable results. Annual average and maximum average N_2O concentrations over specific periods of time (1 hour, 8 hours and 24 hours) are calculated for both simulated scenarios.

III. RESULTS AND DISCUSSION

A. Topographic characteristic of the region

The nitric acid plant is located in the east industrial area of Devnya, Bulgaria. The terrain is mostly lowland with some hilly areas and the elevation varies between 0 and 300 m. The nearest settlement is Povevlyanovo, a suburb of Devnya (to the north). Other settlements in the area are Razdelna, Beloslav and Strashimirovo with elevation almost equal to the elevation of the source site. Settlements to the north from the source such as Slanchevo (elev. 145 m), Kipra (elev. 135 m) and Banovo (elev. 340 m) can be affected by the emission dispersion. These settlements are situated in hilly areas where displacement is higher or almost equal to the geometric height of the source and for that reason certain meteorological conditions may cause increased pollutant concentrations in the ambient air. Fig. 1 presents a topographic map of the source region.

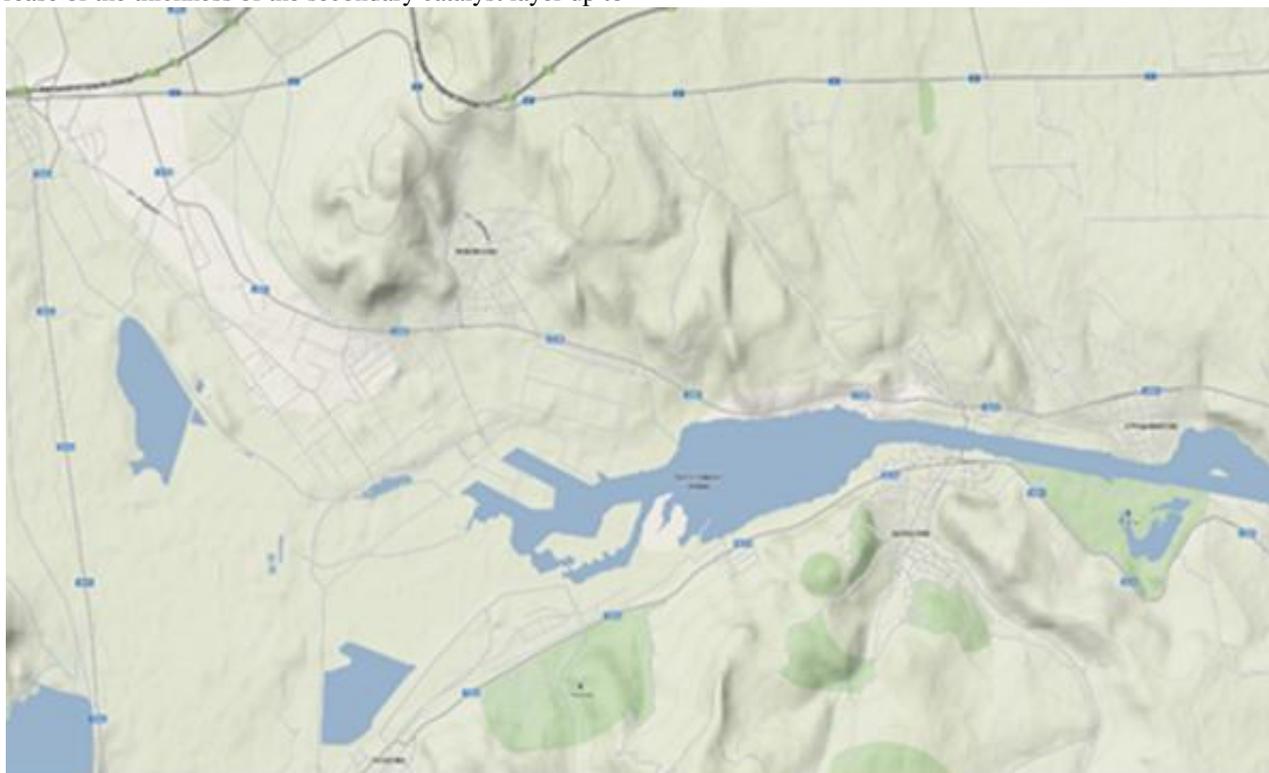


Fig. 1 Topographic map of Devnya region

B. Climate and meteorological conditions of the region

The climate of the source region is typical for its long and dry summer with high coefficient of windless periods and small rainfall quantity. Winter period is short and relatively soft with greater percentage and quantity of rainfall than summer period. There are breeze currents with east – west

direction circulating along Varna Lake and Beloslav Lake. At day time breeze currents come from east while at night they come from west. Moderate winds are typical for the region.

The terrain advantages the formation of inversion fog and considerable pollution of the ambient air. Statistical data indicates that about 60 % of calendar days are foggy.

Fig. 2 presents a wind rose built for the source region for 2013.

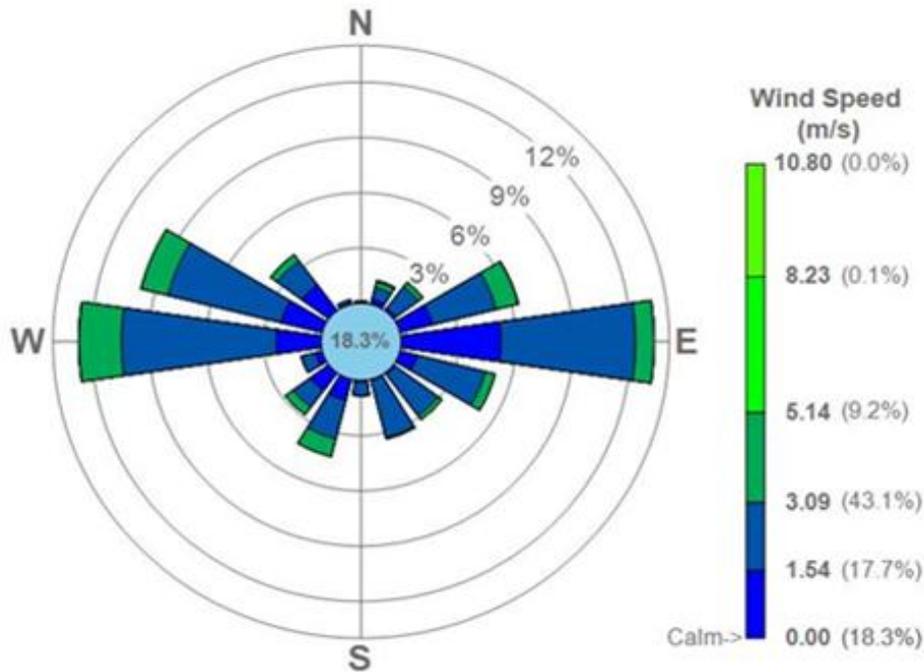


Fig. 2 Wind rose for 2013

As indicated on Fig. 2 most winds come from east and west with speed varying from 1.54 to 3.09 m/s. Winds with speed over 5.14 m/s are very unusual and mostly come from north-northeast. The percentage of windless periods is very low (18.3 %).

C. Results

Within the present research a single point source of N₂O emissions is studied – P1 stack at the nitric acid plant. The height of the stack is 130 m and the diameter is 1.44 m. Due to the fact that N₂O is inert in the troposphere and emissions are expected to expand on long distance from the source the study area is determined with the following proportions – 20000 m on west – east direction and 10000 m on south – north direction. The density of the recipients with a certain N₂O concentration is 41 recipients on x (east) and 21 recipients on y (north) with 500 m step or the total amount of the recipients

is 861.

A simulation of N₂O emission dispersion is done using BREEZE AERMOD software. Annual average N₂O concentrations in the ground atmospheric layer are calculated as well as maximum average N₂O concentrations over specific periods of time (1 hour, 8 hours and 24 hours) for both simulated scenarios.

Table 1 indicates calculation results for peak values of annual average N₂O concentration, recipients’ coordinates and elevation and date/time when peak values are obtained. Fig. 3 and 4 present contours of annual average N₂O concentration (µg/m³) in the ground atmospheric layer for both simulations – at 60 mm thickness of the secondary catalyst layer and at 90 mm thickness of the secondary catalyst layer.

Table 1 Peak values of annual average N₂O concentration (µg/m³)

High	Avg. conc.	UTM		Elev. (m)	Hill Ht. (m)	Flag Ht. (m)	Rec. type	Grid ID
		East (m)	North (m)					
Simulation at 60 mm thickness of the secondary catalyst layer								
1ST	2.53	553791.95	4784610.56	155.40	209.00	2.00	GC	GC50C000

Simulation at 90 mm thickness of the secondary catalyst layer								
1ST	0.79	553791.95	4784610.56	155.40	209.00	2.00	GC	GC50C000

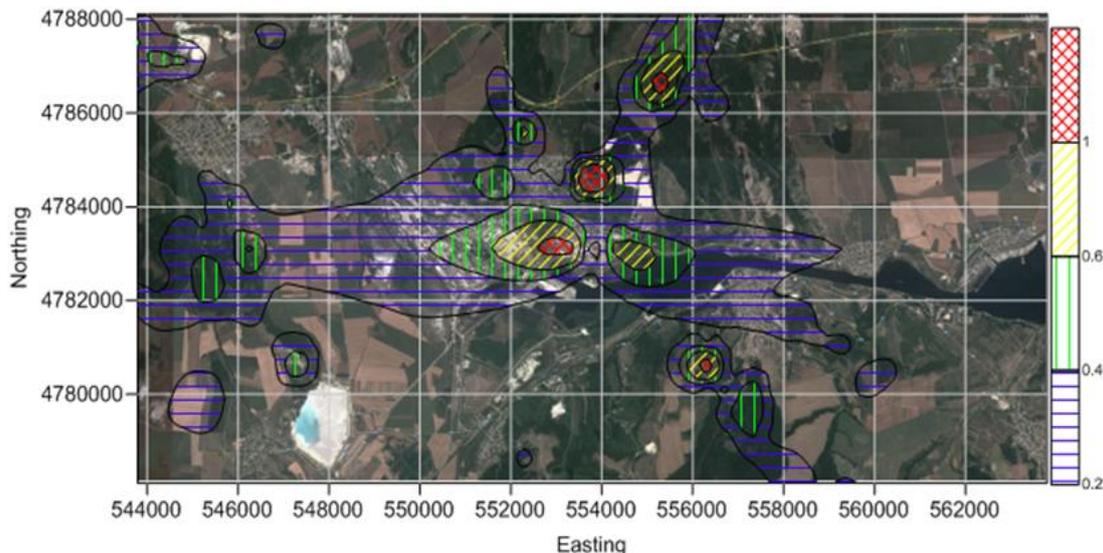


Fig. 3 Annual average N₂O concentration (µg/m³) at 60 mm thickness of the secondary catalyst layer

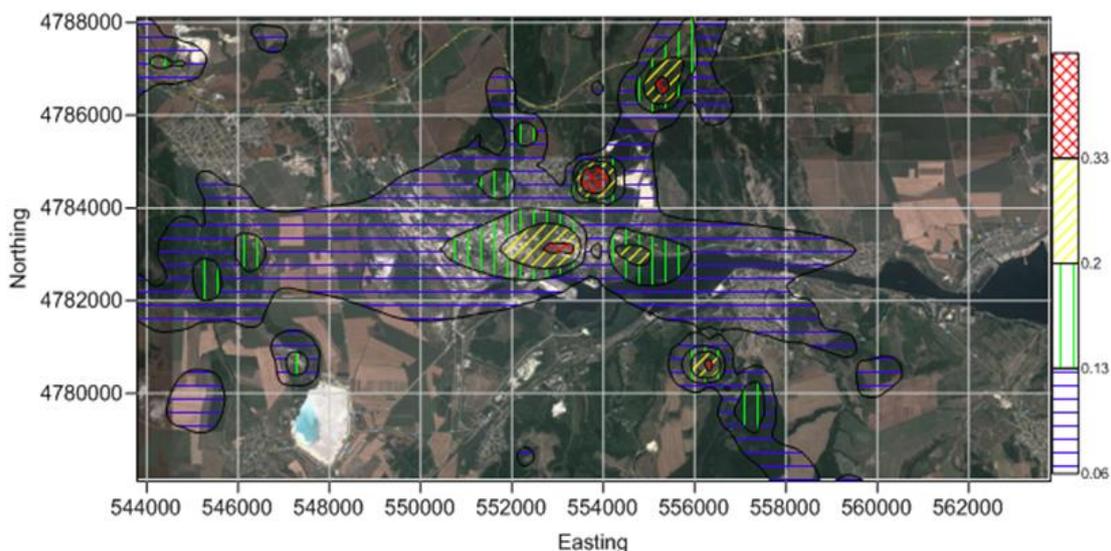


Fig. 4 Annual average N₂O concentration (µg/m³) at 90 mm thickness of the secondary catalyst layer

Table 2 indicates maximum N₂O concentrations (µg/m³) over specific periods of time (1 hour, 8 hours and 24 hours) for both simulated scenarios along with recipients' coordinates and elevation and date/time when peak values are obtained.

Table 2 Maximum N₂O concentration (µg/m³) over specific periods of time (1 hour, 8 hours and 24 hours)

Avg. Per.	High	Type	Value	Date	UTM		Elev. (m)	Hill Ht. (m)	Flag Ht. (m)	Rec. Type	Grid ID
				YYMMDDHH	East (m)	North (m)					
Simulation at 60 mm thickness of the secondary catalyst layer											
1-HR	1ST	Avg. Conc.	1244.23	13/07/02/06	553791.95	4784610.56	155.40	209.00	2.00	GC	GC50C000
8-HR	1ST	Avg. Conc.	307.08	13/07/02/08	553791.95	4782110.56	155.40	209.00	2.00	GC	GC50C000

24-HR	1ST	Avg. Conc.	102.40	13/07/02/24	553291.95	4783610.56	155.40	209.00	2.00	GC	GC50C000
Simulation at 90 mm thickness of the secondary catalyst layer											
1-HR	1ST	Avg. Conc.	388.82	13/07/02/06	553791.95	4784610.56	155.40	209.00	2.00	GC	GC50C000
8-HR	1ST	Avg. Conc.	95.96	13/07/02/08	553791.95	4784610.56	155.40	209.00	2.00	GC	GC50C000
24-HR	1ST	Avg. Conc.	32.00	13/07/02/24	553791.95	4784610.56	155.40	209.00	2.00	GC	GC50C000

As indicated on Table 1, the planned future increase of the secondary catalyst layer thickness from 60 mm to 90 mm leads to prognosis reduction of the annual average N₂O concentration in the ground atmospheric layer over 3 times – from 2.53 to 0.79 µg/m³. Similar reduction trend is observed regarding maximum N₂O concentrations over specific periods of time (1 hour, 8 hours and 24 hours) as prognosis reduction of nearly 69 % is calculated for simulation at 90 mm thickness

of the secondary catalyst layer. Due to equivalent meteorological conditions at both simulated scenarios the maximum hourly N₂O concentration is logically registered at the same recipient point on 2 July at 6.00 a.m. with south wind blowing with speed 2.82 m/s.

Fig. 5 – 10 present the contours of N₂O concentration in the ground atmospheric layer over specific periods of time (1 hour, 8 hours and 24 hours) for both simulated scenarios.

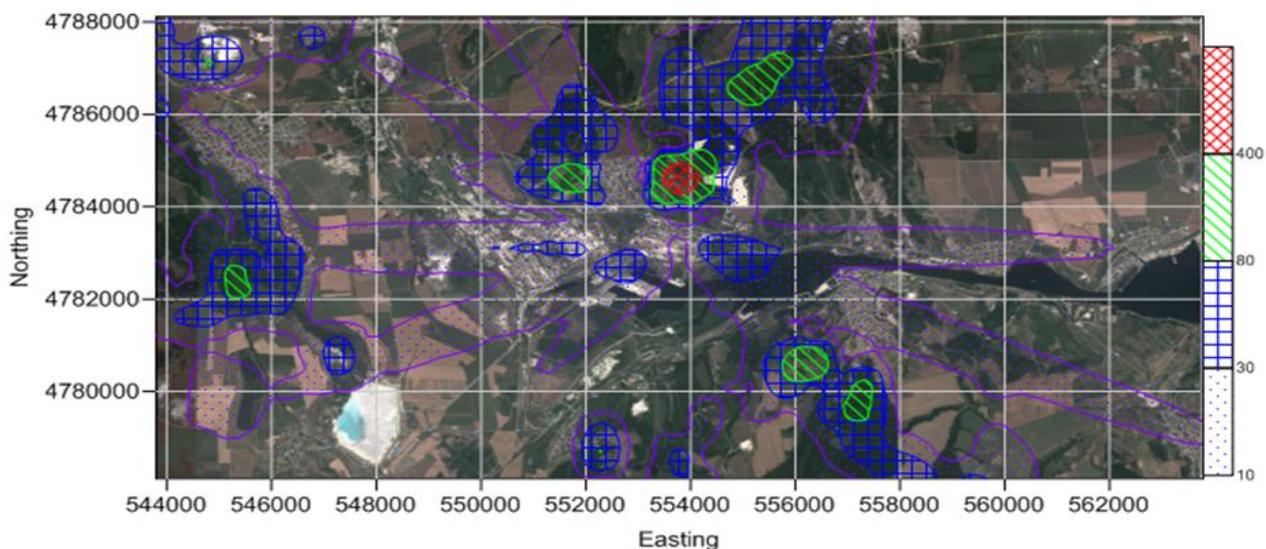


Fig. 5 Hourly average N₂O concentration (µg/m³) at 60 mm thickness of the secondary catalyst layer

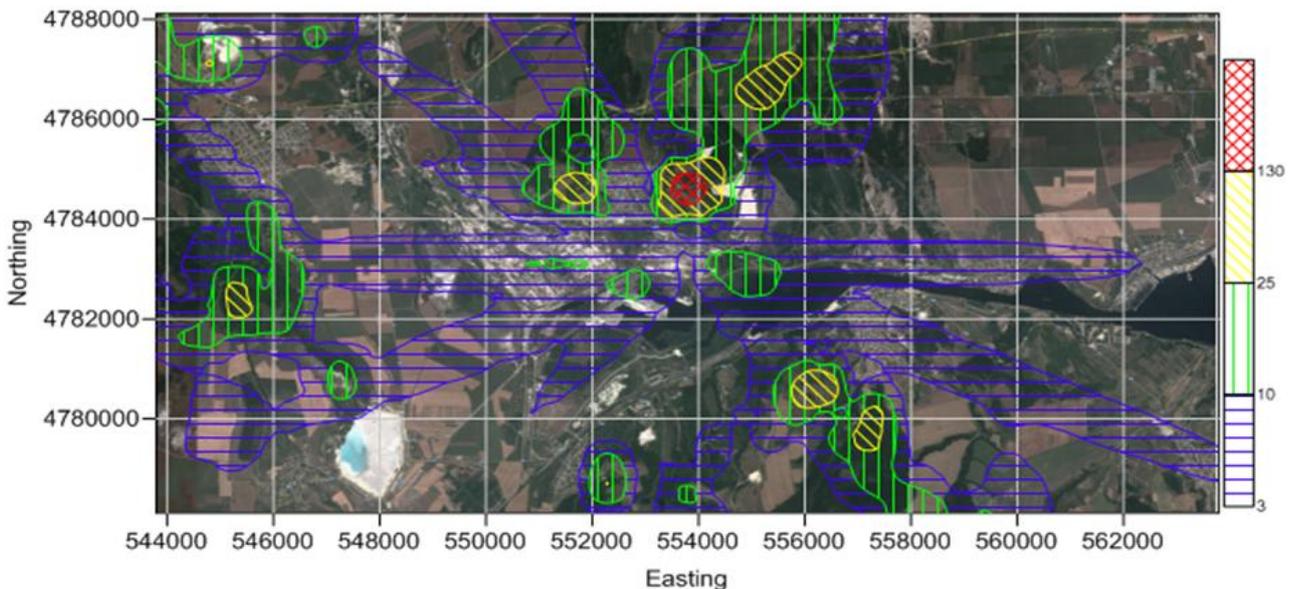


Fig. 6 Hourly average N₂O concentration (µg/m³) at 90 mm thickness of the secondary catalyst layer

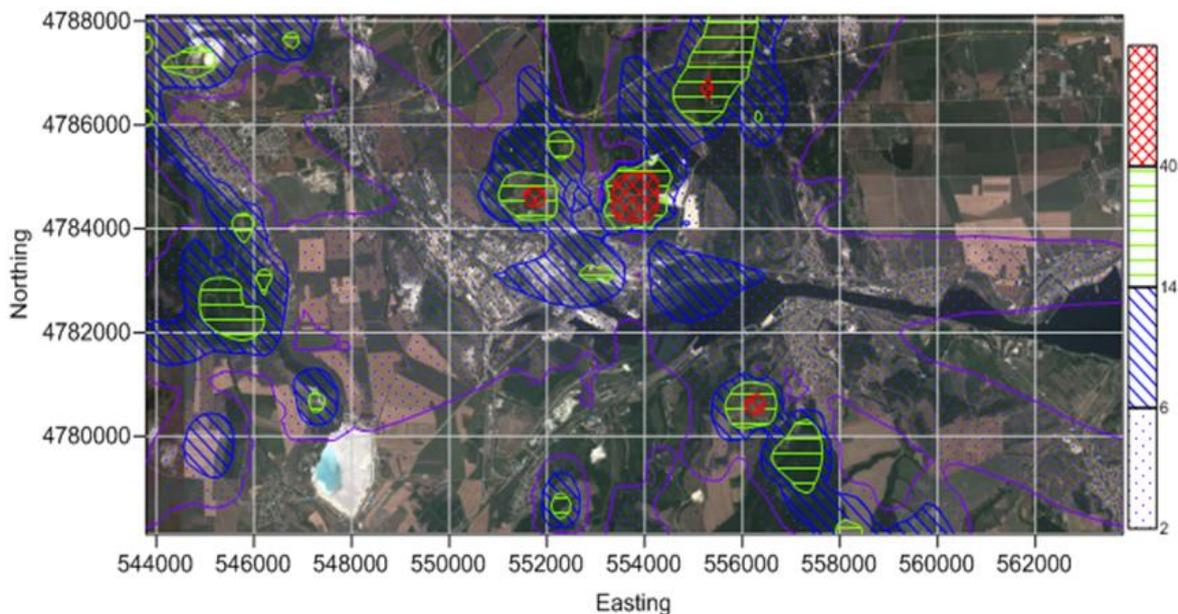


Fig. 7 Eight-hour average N₂O concentration (µg/m³) at 60 mm thickness of the secondary catalyst layer

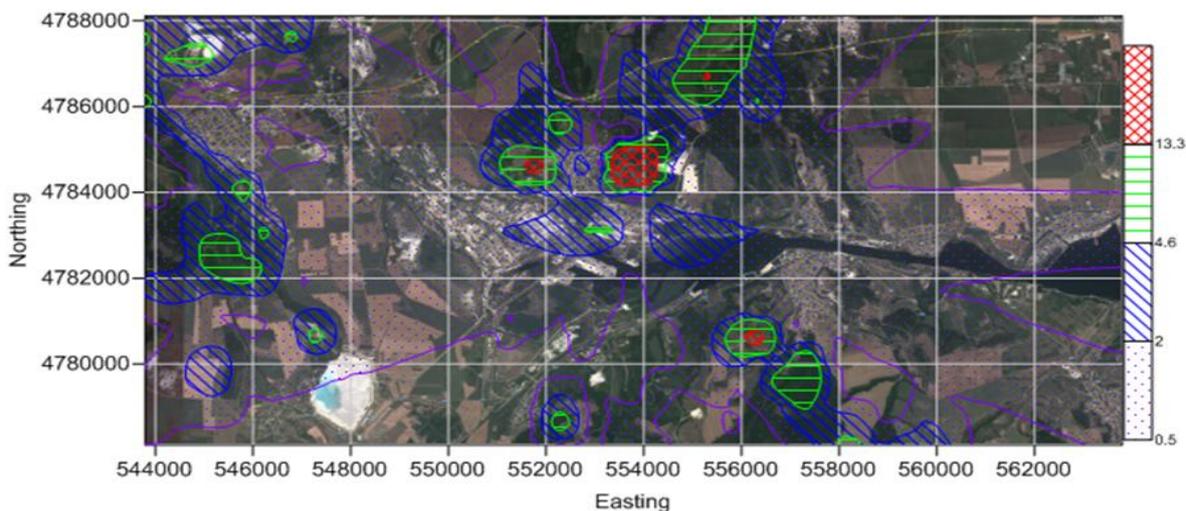


Fig. 8 Eight-hour average N₂O concentration (µg/m³) at 90 mm thickness of the secondary catalyst layer

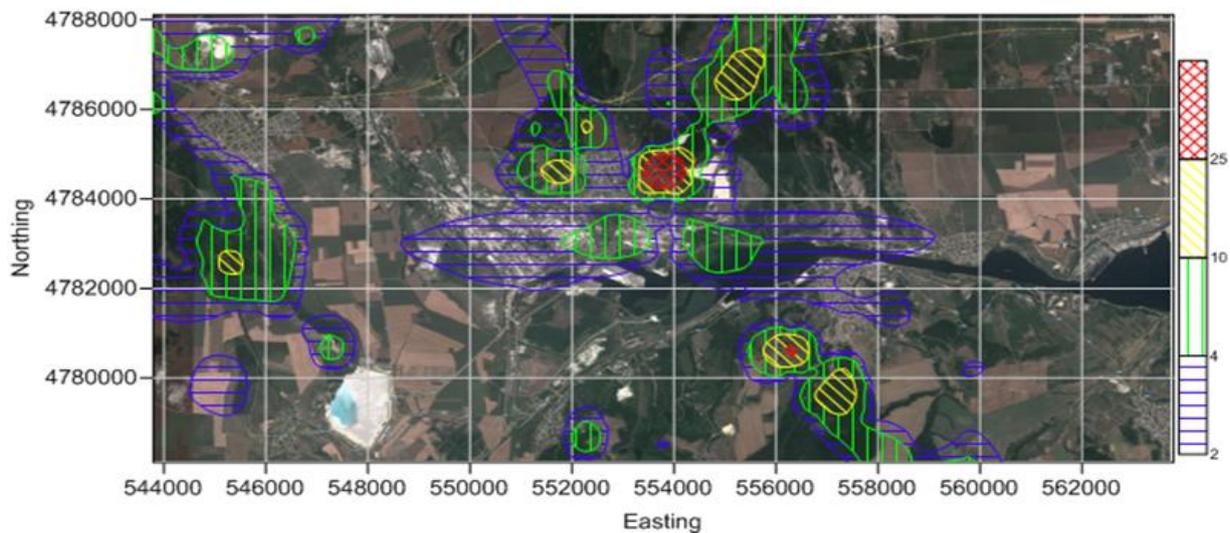


Fig. 9 Daily average N₂O concentration (µg/m³) at 60 mm thickness of the secondary catalyst layer

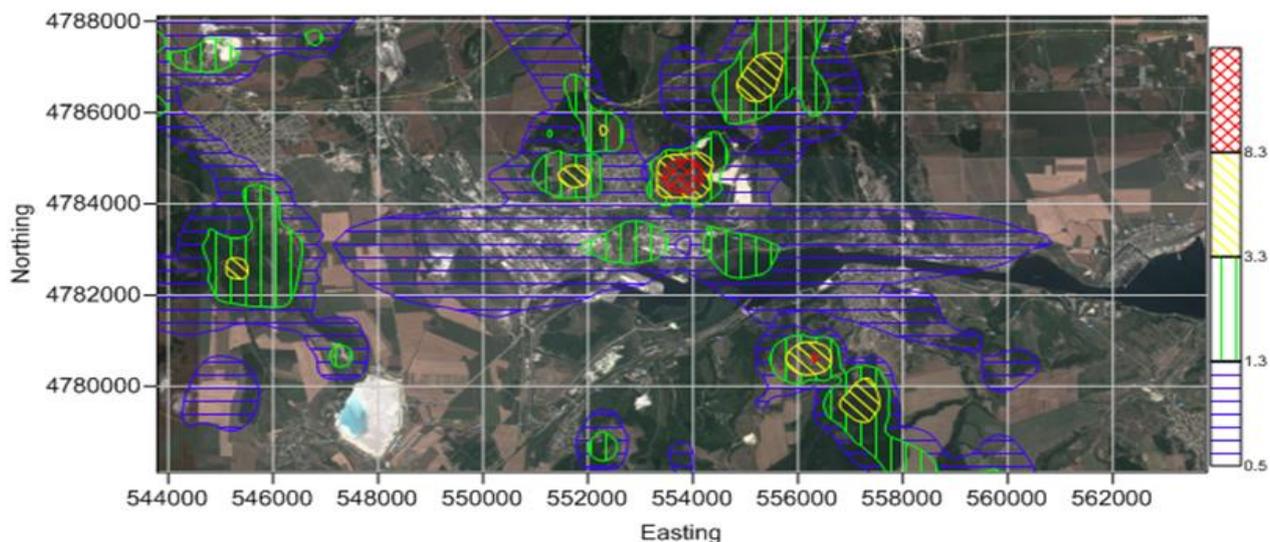


Fig. 10 Daily average N₂O concentration (µg/m³) at 90 mm thickness of the secondary catalyst layer

As indicated on Fig. 5 – 10, the planned future increase of the secondary catalyst layer thickness up to 90 mm leads to reducing the hourly average, eight-hour average and daily average N₂O concentrations in the ground atmospheric layer over 3.2 times due to prognosis reduction of N₂O emissions from the nitric acid plant [26]. Within the present research validated meteorological data for 2013 is used for simulating both scenarios in order to obtain comparable results, therefore the assessment of the planned future increase of the secondary catalyst layer thickness upon the atmospheric N₂O concentration is considered to not depend on the meteorological conditions.

As indicated on Fig. 3 and 4, the contours of the annual average N₂O concentration outline equivalent areas for both simulated scenarios, but the simulation at 90 mm thickness of the secondary catalyst layer presents 3 times lower N₂O concentration within the exposed areas (up to 0.33 µg/m³).

Calculations of the hourly average N₂O concentration in the ground atmospheric layer also indicate equivalent contours of the exposed areas, but the simulation at 90 mm thickness of the secondary catalyst layer presents prognosis N₂O concentration of 130 µg/m³, which is 3 times lower than the hourly average N₂O concentration, simulated at 60 mm thickness of the secondary catalyst layer.

Analogical results are observed regarding N₂O concentrations over the other specific periods of time. The simulation at future increase of the secondary catalyst layer thickness indicates prognosis reduction of N₂O emissions over 3 times, which results in calculating maximum values of 13.3 µg/m³ for the 8-hour average N₂O concentration and 8.3 µg/m³ for the daily average N₂O concentration.

As indicated on Fig. 5 – 10 and Table 2, all peak values are registered at the same recipient point on the grid due to the specific local topography of the source region as the influence of the meteorological conditions is eliminated by using equivalent meteorological data for both simulated scenarios. All maximum N₂O concentrations over specific periods of time (1 hour, 8 hours and 24 hours) for both scenarios are registered at the same point, situated near a hilly area, 760 m away on the east from the nearest settlement (Povelyanovo). Research results clearly indicate that typical

terrain like low hills and low valleys affect considerably the dispersion of atmospheric pollutants even at lowland areas.

IV. CONCLUSION

Analysis of the research results indicates a significant reduction of atmospheric N₂O concentration for simulation at 90 mm thickness of the secondary catalyst layer – 69 % reduction of prognosis annual average, hourly average, 8-hour average and daily average N₂O concentrations is calculated towards their relevant values at 60 mm thickness of the secondary catalyst layer, both scenarios being simulated under the same meteorological conditions. Besides the reduction of atmospheric N₂O concentration, a considerable reduction is registered regarding the atmospheric areas of N₂O emission dispersion. Both simulated scenarios outline equivalent atmospheric areas of dispersion but the simulation at 90 mm thickness of the secondary catalyst layer indicates that the maximum N₂O concentrations over every specific period of time are 3 times lower than their respective values at 60 mm thickness of the secondary catalyst layer. Prognosis models indicate that all maximum N₂O concentrations are registered at the same point, situated close to the nearest settlement therefore the prognosis reduction of atmospheric N₂O concentration affects positively the ambient air quality in the region. Research results illustrate the direct connection between the thickness of the secondary catalyst layer and the reduction potential of the decomposing catalyst and may be used for prognosis assessment of atmospheric N₂O concentration in the source region. The prognosis modeling of N₂O emission reduction by increasing the thickness of the secondary catalyst layer is an assessment tool for calculating the contribution of N₂O emissions from nitric acid production to the overall greenhouse gas emissions of all Member States to the United Nations Framework Convention on Climate Change over the following commitment periods [40].

Efficient reduction of N₂O emissions from nitric acid production leads to reducing the concentration of N₂O in the ground atmospheric layer and is proved to be an effective tool to combat the adverse changes of the climate system and move to a competitive low carbon economy [41]-[42].

REFERENCES

1. The Kyoto Protocol to the United Nations Framework Convention on Climate Change, 1998
2. European Environment Agency. Annual European Union greenhouse gas inventory 1990 – 2012 and inventory report 2014. EEA Technical report No 9 / 2014, Copenhagen, 2014
3. Ravishankara A. R., Daniel J. S., Portmann R. W. Nitrous oxide: The dominant ozone-depleting substance emitted in the 21st century. *Sci.*, 326 (5949), 123-125, 2009
4. Intergovernmental Panel on Climate Change. Climate Change 2014 – synthesis report. Fifth Assessment Report of the Intergovernmental Panel on Climate Change. IPCC, Geneva, 2014
5. Ministry of Housing, Spatial Planning and the Environment. Dutch notes on BAT for the production of nitric acid, The Hague, 1999
6. Agency for Energy and the Environment. Reduction of nitrous oxide in the nitric acid industry. Novem, Utrecht (The Netherlands), 2001
7. European Commission. Integrated Pollution Prevention and Control. Reference Document on BAT for the manufacture of large volume inorganic chemicals – ammonia, acids and fertilizers, 2007
8. Stefanova M. Industrial methods for nitrous oxide emission reduction. *Ecological Engineering and Environment Protection*, 12 (3-4), 89-100, 2013 [In Bulgarian]
9. Perez-Ramirez J., Kapteun F., Schoffel K., Moulijn J. A. Formation and control of N₂O in nitric acid production. Where do we stand today? *Appl. Catal. B-Environ.*, 44 (2), 117-151, 2003
10. Komvokis V. G., Marti M., Delimitis A., Vasalos I. A., Triantafyllidis K. S. Catalytic decomposition of N₂O over highly active supported Ru nanoparticles (≤3 nm) prepared by chemical reduction with ethylene glycol. *Appl. Catal. B-Environ.*, 103 (1-2), 62-71, 2011
11. Dai C., Lei Z., Wang Y., Zhang R., Chen B. Transfer and reaction performances of selective catalytic reduction of N₂O with CO over monolith catalysts. *Chin. J. Chem. Eng.*, 21 (8), 835-843, 2013
12. Dacquain J. P., Lancelot C., Dujardin C., Da Costa P., Djega-Mariadassou G., Beauvier P., Kaliaguine S., Vaudreuil S., Royer S., Granger P. Influence of preparation methods of LaCoO₃ on the catalytic performances in the decomposition of N₂O. *Appl. Catal. B-Environ.*, 91 (3), 596-604, 2009
13. Wen B., Ma J. H., Chen C. C., Ma W. H., Zhu H. Y., Zhao J. C. Supported noble metal nanoparticles as photo/sono-catalysts for synthesis of chemicals and degradation of pollutants. *Sci. China Chem.*, 54 (6), 887-897, 2011
14. Haibo Zhou, Zhen Huang, Chao Sun, Feng Qin, Desheng Xiong, Wei Shen, Hualong Xu. Catalytic decomposition of N₂O over Cu_xCe_{1-x}O_y mixed oxides. *Appl. Catal. B-Environ.*, 125, 492-498, 2012
15. Amrousse R., Katsumi T. Substituted ferrite M_xFe_{1-x}Fe₂O₄ (M = Mn, Zn) catalysts for N₂O catalytic decomposition processes. *Catal. Commun.*, 26, 194-198, 2012
16. Iwanek E., Krawczyk K., Petryk J., Sobczak J. W., Kaszukur Z. Direct nitrous oxide decomposition with CoOx-CeO₂ catalysts. *Appl. Catal. B-Environ.*, 106 (3-4), 416-422, 2011
17. Rico-Perez V., Parres-Esclapez S., Illan-Gomez M. J., De Lecea C. S. M., Bueno-Lopez A. Preparation, characterisation and N₂O decomposition activity of honeycomb monolith-supported Rh/Ce_{0.9}Pr_{0.1}O₂ catalysts. *Appl. Catal. B-Environ.*, 107 (1-2), 18-25, 2011
18. Pasha N., Lingaiah N., Reddy P. S. S., Prasad P. S. S. Direct decomposition of N₂O over cesium-doped CuO catalysts. *Catal. Lett.*, 127 (1-2), 101-106, 2009
19. Amrousse R., Po-Jul Chang, Choklati A., Friche A., Rai M., Bachar A., Follet-Houttemane C., Hori K. Catalytic decomposition of N₂O over Ni and Mg-Magnetite catalysts. *Catal. Sci. Technol.*, 3, 2288-2294, 2013
20. Haibo Zhou, Peilei Hu, Zhen Huang, Feng Qin, Wei Shen, Hualong Xu. Preparation of NiCe mixed oxides for catalytic decomposition of N₂O. *Ind. Eng. Chem. Res.*, 52 (12), 4504-4509, 2013
21. Gao Y., Luan T., Lu T., Cheng K., Xu H. Performance of V₂O₅-WO₃-MoO₃/TiO₂ catalyst for selective catalytic reduction of NO_x by NH₃. *Chin. J. Chem. Eng.*, 21 (1), 1-7, 2013
22. Amrousse R., Tsutsumi A., Bachar A., Lahcene D. N₂O catalytic decomposition over nano-sized particles of Co-substituted Fe₃O₄ substrates. *Appl. Catal. A-Gen.*, 450, 253-260, 2013
23. Lei Zhigang, Long Aibin, Jia Meiru, Liu Xueyi. Experimental and kinetic study of selective catalytic reduction of NO with NH₃ over CuO/Al₂O₃/Cordierite catalyst. *Chin. J. Chem. Eng.*, 18 (5), 721-729, 2010
24. Ma S. C., Jin X., Wang M. X., Jin Y. J., Yao J. J., Liu W. Experimental study on removing NO from flue gas using microwave irradiation over activated carbon carried catalyst. *Sci. China Tech. Sci.*, 54, 3431-3436, 2011
25. Stefanova M., Chaturkova R. Research of the efficiency of a secondary catalyst for nitrous oxide emission reduction at a nitric acid plant. *Pol. J. Environ. Stud.*, 23 (5), 1875-1880, 2014
26. Stefanova M., Chaturkova R. Technical engineering for catalytic reduction of nitrous oxide emissions. *GSTF Journal of Engineering Technology*, 3 (2), 89, 2015
27. Chaturkova R., Stefanova M. Assessment of the effect of nitrous oxide emissions from nitric acid production upon ambient air quality in Devnya region. *Journal Scientific and Applied Research*, 4, 163-170, 2013
28. Stefanova M., Chaturkova R., Sokolovski E., Ilieva N. Dispersion modeling of nitrous oxide emissions from a nitric acid plant in Devnya region, Bulgaria. *International Journal of Research in Engineering and Technology*, 3 (5), 448-457, 2014
29. Stefanova M., Chaturkova R. Catalytic reduction of nitrous oxide at a nitric acid plant in Bulgaria. *Environ. Prot. Eng.*, 40 (3), 87-97, 2014
30. Vallero D. A. Fundamentals of air pollution. Academic Press, Burlington, MA, USA, 2007
31. Tinsley I. J. Chemical concepts in pollutant behavior. Wiley, NJ, USA, 2004
32. Kaur H. Environmental chemistry. Global Media, Meerut, IND, 2010
33. Bhagi A. K., Chatwal G. R. Environmental chemistry. Global Media, Mumbai, IND, 2010
34. Bailey R. A., Clark H. M., Ferris J. P. Chemistry of the environment. 2nd edition. Academic Press, San Diego, CA, USA, 03/2002
35. Jadhav, H. V., Purohit S. H. Global pollution and environmental monitoring. Global Media, Mumbai, IND, 2008
36. P. Kudesia V., Ritu Kudesia. Air pollution. Global Media, Meerut, IND, 2008
37. Borrego C., Schayes G. Air Pollution modeling and its application. Kluwer Academic Publishers, Secaucus, NJ, USA, 2002
38. Pandurangappa C., Lakshminarayanachari K. Mathematical model for an area source and the point source in an urban area. *International Journal of Research in Engineering and Technology*, 1 (1), 20-28, 2012
39. Abdel Salam H. A. Prediction of pollutants emission dispersion of phosphate fertilizers production facility. *International Journal of Research in Engineering and Technology*, 2 (11), 306-311, 2013
40. Report of the Conference of the Parties on its twentieth session, held in Lima from 1 to 14 December 2014. UN Office, Geneva (Switzerland), 2.2.2015
41. Sinha P. K., Rajesh Kumar. Statistical analysis to investigate the possible impact of climate change on water availability in Letaba river of South Africa. *International Journal of Recent Technology and Engineering*, 3 (6), 41-51, 2015
42. Vijaykumar Kulkarni, Pradip Katti. Policies and strategies for the improvement in energy efficiency in industries – Indian experience. *International Journal of Recent Technology and Engineering*, 2 (2), 159-163, 2013

