Abstract: In this paper Analysis and Design of different Structural elements of the football stadium are presented, with particular emphasis on the Combination of Steel Truss without and with Shell roof cover and its interaction with the underlying reinforced concrete structures. The Football stadium considered for the study is of rectangular plan, with 85 m width and 140 m length and height of 19.5 m. The plan of Football Stadium is generated in AutoCAD 2016 software. The Stadium structure is composed of special moment – resisting framed. Wind velocity is taken as 39 mph and Seismic zone IV in this study. The proposed stadium is analysed using Equivalent static and dynamic approach by Response spectrum and Time History analysis. In analysing the structure, 21 load combinations are used. The grandstand structure is made of reinforced concrete and the roof is of structural steel using Pipe and Tube sections. Dead loads, live loads, wind and seismic loadings data are considered based on IS-875 (PART 1-3) 1987 and IS:1893 (Part 1):2016. IS456:2000 and SP16:1987 code is used for Design of R.C.C components such as Beam, Column, Seating Platform, Footing and IS 800:2007 code is used for Design of End Bearing Plate connection with Truss member. Analysis of truss and other elements is carried out with software program of Staad. Pro V8i SS6 and also the designs are carried out as per provisions of relevant Indian standards. On introduction of Shell-like roof for Open Stadium which is used not only to protect the Game from Glare of Sunshine and Rain but also appears unique and attractive. From the obtained results it is observed that the displacement due to Wind action in both X and Z direction reduces significantly by the introduction of Shell roof. Also, due to RSA and THA there is reduction in the displacement on introduction of Shell-like roof to an Open Stadium.

Keywords: Football Stadium Roof Truss, Shell roof, Wind and Seismic analysis, Staadpro V8i SS6.

I. INTRODUCTION

The Recent advances in science and technology, as well as increasing demands for sports and show buildings and facilities, have sparked new development across the globe. Modern stadiums are distinguished by their universality in terms of the ability to host international sporting events and cultural activities. The goal of providing optimum comfort for spectators tends to be associated with fulfilling the needs of sports technology. One part of the job is to cover stands from sunshine and rain by including sheds, canopies, and roofs into the stadium's structural design. Stadiums are the grand platforms on which legends are born and fans get excitement and inspiration. Stadiums, as fascinating and significant buildings, not only enable but also enhance great shows via strong architecture and creative engineering. Structural designers have been under pressure in recent years to create the most practical, technically innovative, and architecturally renowned sports facilities. The most efficient way to track the technical development of modern stadiums throughout this time period is to look at improvements in the design of their structural roof systems.

The stadium should be modified to shield spectators from rain and blinding light in the event of a strong sun. Although some pretty continuous steady sunlight is typical, shade provided by the roof should be accessible to all open areas for at least a portion of the game, which is not always feasible. The stadium should be built such that all parameters are essentially comfortable, safe, and secure, and that each and every individual has a clear view of the court. The arrangement of seating is provided is continuous the maximum seating can be easily placed in stadium. In recent days, many research scholars have worked on the cover or roofed stadium. Mohini R. Gawande et al [1] carried out the study on Analysis and Design of Roof Tubular Truss for Cricket Stadium and effect of wind action on the long span roof truss which should be minimized using recent technology. The Seismic analysis of the Cantilever truss roof of the stadium have been worked in [2] and the results showed the drift and displacements due the wind load is more when compared to earthquake load. Nonlinear Seismic Analysis of the stadium using viscous dampers is worked out in the literature [3] and the response of the structure is obtained and they found that viscous dampers help in decreasing the displacements by 60%. Dynmic monitoring of the suspension roof of the stadium has been worked in [4] developing a ground assessment of wind action, establish a connection with structural response, and subsequently analysing the influence of wind and temperature on modal parametric variations. In literature [5] the research shows that the spatial truss structure is reasonable and able to meet the building's quality standards. Steel.
Analysis and Design of Stadium with Truss System and Shell Roof Subjected to Wind and Seismic Loading

The present study is to analyse and design the stadium with steel roof truss is aimed to get a better understanding of the stadium structural analysis and design idea for steel roof truss. The Lattice truss is generally used for long span, in which the triangular and N- type frame arrangement taken for work. N and triangular frame arrangement consider the axially loaded member and N-type connection properly distributes the load acting at downward side and is distributed in node to node in whole structure. N-type truss system pattern is stronger than other arrangement for long span. They are more capable to resisting external forces or loads acting on section, to all members nearly uniformly stress. Lattice truss and N-type trusses are proposed to be used for the present study.

II. OBJECTIVES OF THE STUDY
1. To Develop the 3D Model of an Outdoor Stadium Structure with Truss and Shell roof Covering system.
2. To determine the behavior of the stadium structure under Static and Dynamic loading using STAAD. Pro V8i SS6 software.
3. To Design the components of the Outdoor Stadium Structure.

III. METHODOLOGY OF THE STUDY
This particular study includes the 3D model of Outdoor Stadium structure. The Analysis and Design of Stadiums with Truss system and Shell roof is carried out by considering dead loads, live loads, wind loads and seismic loads for the proposed structure. And all the loads will be designed by Indian standard codes with aid of design software STAAD. Pro V8i SS6. In this study
This project mainly emphasizes on wind and seismic analysis of the Stadium structure. The modelling of Stadium has been done on the STAAD. Pro V8i SS6 software for analysis. The parameters after the analysis of the structure such as displacement, base shear and fundamental time period is computed. Here in this thesis, the analysis of structure evaluated in order to find the behavior with Truss system and Shell roof patterns. The seismic zone considered is zone IV and with soil type medium. The modelling of structure is done for Indian Seismic Zone IV, earthquake loading and wind loading are considered in the analysis. For given structure, loading with applied loads includes live load, earthquake load and dead loads are according to Indian Standards. The analysis is taken out by Equivalent Static, Response spectrum and Time History methods using STAAD. Pro V8i SS6 software.

A. Flowchart of the Methodology:
The methodology of the Proposed Stadium structure for the analysis and design using Staadpro V8i SS6 software is as follows

Inputs: Model creation
(Node, Beams, Secondary Beams and Columns)

Defining the material properties of the structure

Defining Supports

Defining loads, Assigning the loads and its combinations on the structure

Analysis and print

Run analysis

Outputs: Axial force (Truss member)

Shear force diagram

Bending moment diagram

Deflections

Design: Reinforced concrete structures
(Beams, Columns, Platform Slabs, Footing)

Roof truss pattern

Shell roof structure

Conclusion

B. Modeling & problem formulation
To model a Stadium Structure in STAAD. Pro V8i SS6, we require some preliminary data to input such as codes for design, material specifications, building specification with the dimensions of each structural component, load case, load patterns & load combination. However, the modelling may differ from case to case. Later a brief procedure of modelling, analysis & design of the building in STAAD. Pro V8i SS6 will be discussed as per the methodology in accordance with problem formulation.

C. Description of the Models:
Model-I: Outdoor Football Stadium without Shell roof cover
Model-II: Outdoor Football Stadium with Shell roof cover

Before Modelling in the Staad Software the plan of the Football stadium is created in the Auto Cad 2016 software by following the standard dimensions of the football stadium is shown in Fig 1. According to the stipulations from FIFA the standard Dimension of the football stadium is 45m-90m width and 90m-120m length. For the study 45m width and 100m length Play court is considered. The 3D Staad model of roof truss stadium without and with Shell roofing is shown below.

D. Dimensions of the stadium
• Overall length of the structure = 140 m
• Overall Width of the structure = 85 m
• Overall height of the structure = 19.5 m
• Length of the Play court = 100 m
• Width of the Play court = 45 m
• Spectator Gallery = 20 m
compound of Lattice type of truss along with N- type truss has been used for the roof and the same has been analysed and designed. The steel truss is designed to be simply supported on the column and the Lattice truss is analysed according to Indian requirements. For the following various parameters, the study of Lattice truss is done on the basis of applicable Indian Standards:

B. Geometry of Roof Truss:
   Roof truss = Lattice Truss
   Span of Truss = 32.14 m
   Spacing of Truss = 6.67 m

C. Shape and Dimensions of a single Lattice Roof Truss:
   The Shape of the proposed Lattice truss and Dimension is show in Fig 4 and 5 respectively

D. Assigning of Section Properties:
   The section properties are assigned using Staad for the single lattice roof truss for both the Models which is given in Table I and Table II respectively, and the assigning of the property to Top chord, Intermediate Chord, Bottom Chord and Purlin are shown.

<p>| Table I. Section properties of Truss members (Model-I) |
|----------------|----------------|----------------|----------------|
| Model-1 (Stadium without Shell roof) |</p>
<table>
<thead>
<tr>
<th>Member</th>
<th>Material</th>
<th>Section</th>
<th>Thickness</th>
</tr>
</thead>
<tbody>
<tr>
<td>Top Chord</td>
<td>Steel</td>
<td>PIP 200 H</td>
<td>6 mm</td>
</tr>
<tr>
<td>Intermediate Chord</td>
<td>Steel</td>
<td>PIP 150 H</td>
<td>6 mm</td>
</tr>
<tr>
<td>Bottom Chord</td>
<td>Steel</td>
<td>PIP 250 H</td>
<td>8 mm</td>
</tr>
<tr>
<td>Purlin</td>
<td>Steel</td>
<td>TUB 1001005</td>
<td>5 mm</td>
</tr>
<tr>
<td>Column</td>
<td>Concrete</td>
<td>1500 mm x 1500 mm</td>
<td></td>
</tr>
<tr>
<td>Beam</td>
<td>Concrete</td>
<td>300 mm x 600 mm</td>
<td></td>
</tr>
</tbody>
</table>
Table II Section properties of Truss members (Model-II)

<table>
<thead>
<tr>
<th>Model-II (Stadium with Shell roof)</th>
<th>Member</th>
<th>Material</th>
<th>Section</th>
<th>Thickness</th>
</tr>
</thead>
<tbody>
<tr>
<td>Top Chord</td>
<td>Steel</td>
<td>PIP 250 H</td>
<td>6 mm</td>
<td></td>
</tr>
<tr>
<td>Intermediate Chord</td>
<td>Steel</td>
<td>PIP 150 H</td>
<td>6 mm</td>
<td></td>
</tr>
<tr>
<td>Bottom Chord</td>
<td>Steel</td>
<td>PIP 350 H</td>
<td>8 mm</td>
<td></td>
</tr>
<tr>
<td>Purlin</td>
<td>Steel</td>
<td>TUB 1001005</td>
<td>5 mm</td>
<td></td>
</tr>
<tr>
<td>Column</td>
<td>Concrete</td>
<td></td>
<td>1500 mm x 1500 mm</td>
<td></td>
</tr>
<tr>
<td>Beam</td>
<td>Concrete</td>
<td></td>
<td>300 mm x 600 mm</td>
<td></td>
</tr>
</tbody>
</table>

Fig.6 Assigning the section properties for Top Chord

Fig.7 Assigning the section properties for Intermediate Chord

Fig.8 Assigning the section properties for Bottom Chord

Fig.9 Assigning the section properties for Purlin

The RCC Component such as Column and Beam property are shown in the below Fig 10 and 11 respectively

Fig.10 Assigning the properties for RCC Column

Fig.11 Assigning the properties for RCC Beam

E. Shell Roof Truss Configuration:
The typical Shell roof truss is shown in the below Fig 12 and the section properties of the same is tabulated in underneath Table III

F. Geometry of Shell Roof Truss:
Span of Truss = 25 m.
Spacing of Truss = 6.67 m

Fig.12 Typical Shell Roof Truss
Table III Section properties of Shell Roof Truss members

<table>
<thead>
<tr>
<th>Model-II (Stadium with Shell roof)</th>
<th>Material</th>
<th>Section</th>
</tr>
</thead>
<tbody>
<tr>
<td>Top Chord</td>
<td>Steel</td>
<td>PIP 2191 H</td>
</tr>
<tr>
<td>Intermediate Chord</td>
<td>Steel</td>
<td>PIP 1524 H</td>
</tr>
<tr>
<td>Bottom Chord</td>
<td>Steel</td>
<td>PIP 2191 H</td>
</tr>
<tr>
<td>Purlin</td>
<td>Steel</td>
<td>TUB 90905</td>
</tr>
</tbody>
</table>

G. Loading:
1. Dead Loads:
   Dead loads considering the weight of all material and fixed components incorporated into the stadium structure, as per IS:875 (Part-I) –1987 has been considered to calculate dead load.

2. Live Loads:
   Live loads are calculated as per IS:875 (Part-II) –1987 shall be the maximum loads normal by the intended use or utilized. They may be considering the tentative load taken in fully or partially in place in roof area or not present at every time.

Calculation of Live Load on Truss member:
As per clause 4.1 Table 2 of IS: 875 (part-2) -1987
θ = 5.33°
Live load on truss = 0.75 kN/m² > 0.4 kN/m²

3. Wind Loads:
The calculation of wind design force is taken as per IS:875 (Part III) - 2015.

Calculation of Wind Load:
As per clause 5.3 of IS875 (Part 3)- 2015, we have
Vz = Vb x k1 x k2 x k3
Wind Zone = II
Basic wind speed value Vb = 39 m/s
K1 = 1.06
K2 = 0.97
K3 = 1
Design wind speed (Vz) = Vb x k1 x k2 x k3
= 39 x 1.06 x 0.97 x 1
= 40.09 m/s

Calculation of Wind Pressure:
Wind pressure pz is calculated by using the formula as per 5.4 of IS 875: 2015 (Part-III)
pz = 0.6 Vz²
= 0.6 x (40.09)² = 964.32 N/sq.m
= 0.964 kN/sq.m

Calculation of Design Wind Pressure:
Pd = k d x k a x k c x pz
k d = 0.90
k a = 0.92
k c = 0.9
Pd = k d x k a x k c x pz
= 0.9 x 0.92 x 0.9 x 0.964
= 0.718 kN/m²

Design wind pressure shall not be less than 0.7 x Pz
= 0.7 x 0.964
= 0.674 kN/sq.m
0.718 kN/sq.m > 0.674 kN/sq.m Hence OK

Calculation of Wind Pressure Coefficients:
F= (Cpe – Cpi). A. pd

Calculation of External Pressure Coefficients:
Let θ be the inclination of the roof (θ)
Tan (θ) = rise / half of span
θ = 5.33
h = 19.5 m, w = 85 m
h/ w = 19.5 / 85
= 0.22 < 0.5
Cpe condition h/w < ½

Table IV External Pressure Coefficients

<table>
<thead>
<tr>
<th>Cpe</th>
<th>Wind angle = θ°</th>
<th>Wind angle = 90°</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>EF</td>
<td>GH</td>
</tr>
<tr>
<td>-0.91</td>
<td>-0.4</td>
<td>-0.8</td>
</tr>
</tbody>
</table>

Calculation of Internal Pressure Coefficients:
Structures with openings larger than 20% the value of internal pressure coefficient is taken as Cpi = +0.7 and - 0.7

Table V Wind Load calculation

<table>
<thead>
<tr>
<th>Wind angle</th>
<th>Total pressure = (Cpe – Cpi) pz</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>Cpe</td>
</tr>
<tr>
<td>Windward</td>
<td>-0.91</td>
</tr>
<tr>
<td>Leeward</td>
<td>-0.4</td>
</tr>
</tbody>
</table>

Maximum wind load in Windward direction = -1.5424 kN/m² and Maximum wind load in Leeward direction = -1.0604 kN/m² where, (-) indicates uplift pressure also called as Suction. The action of wind on Windward and Leeward face of the structure in both X and Z direction is shown in Fig 13, 14, 15 and 16 respectively.

Fig.13 Wind Load acting on Windward face X direction

Fig.14 Wind Load acting on Leeward face X direction
4. Seismic Load:
In accordance with IS1893-2016 (part I) the parameters used for Seismic analysis of the structure are given in the Table VI. The action of earthquake load in X+, X-, Z+ & Z- is shown in fig 17, 18, 19 and 20 respectively.

Table VI: Parameters for Seismic analysis

<table>
<thead>
<tr>
<th>Earthquake Zone</th>
<th>IV</th>
</tr>
</thead>
<tbody>
<tr>
<td>Zone factor (Z)</td>
<td>0.36</td>
</tr>
<tr>
<td>Response Reduction Factor (R)</td>
<td>5 (S.M.R.F.)</td>
</tr>
<tr>
<td>Importance Factor (I)</td>
<td>1.5 (Very Important Building)</td>
</tr>
<tr>
<td>Soil Type</td>
<td>II (Medium Soil)</td>
</tr>
<tr>
<td>Type of Structure</td>
<td>I</td>
</tr>
<tr>
<td>Diaphragm Damping for steel</td>
<td>2%</td>
</tr>
<tr>
<td>Diaphragm Damping for concrete</td>
<td>5%</td>
</tr>
</tbody>
</table>

After adding the Seismic load in both X and Z direction the method of seismic analysis is applied such as RSA and THA which is shown in below Fig 21 and Fig 22.
After creation of model and assigning the properties, the model has been checked and obtained zero errors is shown in the below Fig. 23. The unity check ratio has been checked for the typical steel truss members and Shell members and were in the permissible limit. The same is shown in the below Fig 24 and Fig 25.

V. RESULTS AND DISCUSSION

After the completion of analysis of the structure the results are extracted as stated, now these results are tabulated accordingly and the effect of various parameters are observed and discussed. This project focuses on the wind and seismic behavior on the structure hence the parameters are tabulated and are discussed. Then latter the Manual design of Beam, Column, Seating Platform, Footing and Base Plate connection is done with the help of forces obtained from Staad Analysis.

A. Generalize co-ordinates in Staad.pro V8i SS6:

As discussed, earlier Staad.pro V8i SS6 uses Finite Element Method (FEM) to analyse the various unknowns in a structural system. It is necessary to understand the generalize coordinate system, with respect to which the results are generated so that the behavior of structural system can be studied. Figure 26 shows the reference axis in Staad.pro V8i SS6.

B. Wind Analysis Results:

Displacement: The Displacements due to wind load action in X and Z direction at particular nodes for both Model-I and Model-II i.e., Stadium without shell roof and with Shell roof.

The Displacement due to Wind action in X direction on both Model-I and Model-II at a particular node have been shown in Fig. 27 and Fig. 28.

From the graph at node number 5567 the displacement in X-direction is maximum i.e., 0.018 mm for Model-I whereas at same node the displacement is 0.002 mm for Model-II. Hence the Displacement for Model-II is decreases by 88.88 % when compared to Model-I.
From the graph at node number 5567 the displacement in Z-direction is 0.468 mm for Model-I whereas at same node the displacement is 0.107 mm for Model-II. Hence the Displacement for Model-II is decreases by 77.13 % when compared to Model-I.

**Drift:** The Drift due to wind load action in X and Z direction at particular nodes for both Model-I and Model-II is shown in Fig. 29.

From the graph at Height 12.56 m the drift in X-direction is maximum i.e., 9.981 mm for Model-I whereas at same Height the drift is 0.957 mm for Model-II. Hence the Drift for Model-II is decreases by 90.41% when compared to Model-I and from the graph at Height 12.56 m the drift in Z-direction is 1.112 mm for Model-I whereas at same Height the drift is 0.938 mm for Model-II. Hence the Drift for Model-II is decreases by 15.64% when compared to Model-I.

**Displacement for Model:**

- Model-I: Z direction is 0.489 mm for Model-I whereas at same Height the drift is 0.527 mm for Model-II. Hence the Drift for Model-II decreases by 4.35% when compared to Model-I.

**Time Period:**

- Model-I: The time period is 0.74467 sec whereas for Model-II is 0.78906 sec, Hence the Time period for Model-II is increases by 5.12% when compared to Model-I.

### Design Seismic Base Shear:

During a lateral ground motion, the structure gets displaced from its mean position due to the application of lateral forces at every story height the algebraic addition of these lateral forces at the base of the structure gives base shear. It should be noted that structure gets displaced in both directions hence base shear in each direction is calculated i.e., in X and Z direction in accordance with the generalize coordinate. The underneath Fig 31 demonstrates the estimations of seismic base shear of both the models, by the 2 distinctive examination techniques like, RSA, THA the base shear likewise relies on the state of the site on which the structure needs to stand.

**Story Drift:** The results of story drift given below are due to worst load combination with partial safety factor. But the design of all structural members in STAAD have been passed in software which is for load combination with partial safety factor 1, thus this implies that story drifts are within the limits. The story drift in X and Z directions are tabulated in underneath Fig 32 for the both models, these qualities are acquired by performing examination by various techniques utilizing STAAD.

From the graph it is observed that the time period for Model-I is 0.74467 sec whereas for Model-II is 0.78906 sec, Hence the Time period for Model-II is increases by 5.12% when compared to Model-I.

**Time Period**

- Model-I: The time period is 0.74467 sec whereas for Model-II is 0.78906 sec, Hence the Time period for Model-II is increases by 5.12% when compared to Model-I.

### Design Seismic Base Shear:

- Model-I: The seismic results for both models discussed are time period, base shear, displacement, story drift. These parameters are of core importance for the structure to be an earthquake resistant.

#### Time Period:

Time period is defined as “In an earthquake it is a time required by a structure (as a whole) to complete one oscillation from its mean position”. Here in STAAD in a dynamic analysis of response spectrum 6 modes of oscillation is considered in which 90% and above accuracy is achieved. It is quite obvious that, if time period is less the building will take less time to oscillate and vice versa. Less time period of a structure will imply good resistance towards an earthquake. It is only the undamped free vibration of the structure. The Fig 30 underneath speaks about the estimations of time period acquired by the investigation utilizing STAAD for Model-I and Model-II respectively.
Hence the Story Drift for Model-II is decreases by 4.30 % when compared to Model-I.

**Displacement:** During a ground motion due to lateral stiffness of the column the story is displaced with respect to ground. This lateral distance with which the floor is displaced during a ground motion of an earthquake is called story displacement. The limit is given by \( H/150 \) where \( H \) = Height of the structure as per clause 5.6.1 IS 800:2007 and all the obtained results for Model-I and Model-II were within the limit. with respect to the generalize coordinate shown in Fig. 33 and Fig.34.

**Displacement:**

During a ground motion due to lateral stiffness of the column, the story is displaced with respect to ground. This lateral distance with which the floor is displaced during a ground motion of an earthquake is called story displacement. The limit is given by \( H/150 \) where \( H \) = Height of the structure as per clause 5.6.1 IS 800:2007 and all the obtained results for Model-I and Model-II were within the limit. with respect to the generalize coordinate shown in Fig. 33 and Fig.34.

**Fig.33 Displacement due to Seismic Action Model-I**

**Fig.34 Displacement due to Seismic Action Model-II**

From the graph at node number 6356 the Story displacement due to ESA in X-direction is 1.123 mm for Model-I whereas at same node the displacement is 2.049 mm for Model-II. Hence the Displacement for Model-II is increases by 45.19 % when compared to Model-I.

From the graph at node number 6356 the Story displacement due to ESA in Z-direction is 1.503 mm for Model-I whereas at same node the displacement is 0.008 mm for Model-II. Hence the Displacement for Model-II is decreases by 99.46 % when compared to Model-I. Also, from the graph it is observed that at the same node Story displacement due to RSA and THA in X direction for Model-II is decreases by 18.87 % and increases by 8.33 %, respectively when compared to Model-I.

From the graph it is observed that at the same node Story displacement due to RSA and THA in Z direction for Model-II is decreases by 19.19 % and 9.61 % respectively when compared to Model-I.

D. **DESIGNS:**

The design of structural components such as Beam, Column, Seating Platform Slab, Footing and Base Plate Connection is carried out and discussed below.

**Design of RC Beam:**

Typical design details of RC Beam with No 32871 shown in Fig. 35 are presented in this section.

**Fig. 35 RC Beam Number 32871**

Beam Section provided (300 x 600)

- \( F_{ck} = 30 \) Mpa
- \( F_y = 500 \) Mpa

Forces from Staad

- Max support Moment = 255 kNm
- Mid span moment = 127 kNm
- shear force = 205 KN

The Shear force and Bending Moment diagrams are shown in Fig. 36 & 37 respectively. The design details of the beam are given in Fig.38.

**Fig. 36 Shear force diagram for Beam 32871**

**Fig. 37 Bending moment diagram for Beam 32871**

**Fig. 38 SCHEDULE OF BEAM**

- Top Bars: 4 B/A 8 mm
- Bottom Bars: 4 B/A 8 mm
- Tension Strips: 2 Hoop 12 mm
- Stiffeners: S 6 mm
- Stirrups: 4 B/A 8 mm
- L-Beam: 125 mm x 125 mm x 12 mm x 12 mm
- Welded Wire: 6,3 mm x 50 m
Analysis and Design of Stadium with Truss System and Shell Roof Subjected to Wind and Seismic Loading

Design of Column:
Typical design details of RC Column with No 24765 shown in Fig. 39 Axial force and BM values are shown in Fig 40 and are presented in this section.

Fig.38 Reinforcement Details of Beam section

Fig.39 RC Column 24765

Design of Footing:
Design of Isolated footing:
Axial Force 1756.305 kN
Moment in X direction = 5.415 kNm
Moment in Z direction = 1701.74 kNm
P = 1170.87 kN
SBC=220 kN/m2
SBC = 220 X 1.25 = 275 kN/m2
Column size = 1500 mm x 1500 mm
Area of Footing
A = (Total load)/SBC = (1170.87*1.1)/275 = 4.68 m^2
Provide Square Footing of Size = \sqrt{4.68} = 2.16 m
Provided area = 3.5 m x 5 m
The design details of the isolated footing is given in Fig 42.

Fig.40 Axial force and BM values for Column 24765

Forces from Staad:
Column Dimension = 1500 mm x 1500 mm
Grade of concrete = 30 N/mm2
Characteristic strength of reinforcement = 500 N/mm2
The design details of the Column is given in Fig 41.

Fig.41 Reinforcement Details of Column section

Fig.42 Footing Details

Design of Seating Platform Slab:
The Seating Platform is a huge structure designed to carry the superimposed load of furniture and audience. The furniture is arranged on a number of successive steps so that view of the audience is not obstructed. These steps along with the waist slab are supported on rackers which on turn are supported on wall on one side and the fulcrum girder on the other side. The treads are normally kept between 900 to 1100 mm and the risers between 100 to 125 mm. The superimposed load may vary between 4 to 5 kN/m^2. The General Layout of Seating Platform is shown in the Fig.43

Live Load inclusive of furniture 5 kN/m^2.
Horizontal tread = 1 m
Rise = 120 mm
The depth of fulcrum girder = 1 m.
Width of Gangway = 1 m
Density of Concrete = 25kN/m^3

Fig.43 General Layout of Seating Platform Embargo
Loading on Racker Beam, SFD and BMD is shown in the below Fig 44.

The reinforcement details of the T beam is given in Fig. 45.

The details of reinforcement of Seating Platform are shown in Fig. 46 & 47.

Design of Base Plate
The Bottom chord member of Truss is supported on RCC Column 1500 mm x 1500 mm.
Axial force (DL+LL) = 1670.233 kN
Uplift pressure due to wind load = 158.813 kN
Bending Moment = 1455.969 kNm
Grade of concrete (fck) = 30 N/mm²
Diameter of Bottom Chord = 350 mm
Thickness of Bottom Chord = 8 mm
Supported on RCC Column = 1500 mm x 1500 mm
Class of Bolts for all connections = 8.8
The Dimension of the Base plate provide is given in Fig. 48.

The connection of the Base plate to RCC Column through Anchor Bolts is shown in Fig. 49 and the truss member connection to RCC Column is shown in Fig. 50.
Analysis and Design of Stadium with Truss System and Shell Roof Subjected to Wind and Seismic Loading

VI. CONCLUSION

Following Conclusions are drawn from the results of the Project work:
1. Introduction of Shell-like roof for Open Stadium which is used not only to protect the Game from Glare of Sunshine, Rain etc but also appears unique and attractive.
2. The Fundamental Time Period for Model-II i.e., Stadium with Shell roofing is found to be Increasing due to increase in height when compared to Model-I i.e., Stadium without Shell roofing.
3. From the results it is observed that the displacement due to Wind action in both X and Z direction reduces significantly by the introduction of Shell roof i.e., Model-II in comparison with Model-I (Stadium without Shell roof).
4. The Drift due to Wind action in both X and Z direction for Model-II reduces when compared to Model-I.
5. There is increase in Base Shear for Model-II when compared with Model-I due to introduction of Shell roof due to increase in Seismic weight of the structure.
6. The Story Drift due to Seismic action in both X and Z direction for Model-II reduces significantly when compared to Model-I.
7. Both RSA and THA techniques gave reduced Story displacement values for Model-II when compared to Model-I in contrast to ESA which gave reduced displacement values for Model-II in Z direction only.

VII. SCOPE FOR FURTHER STUDY

1. Optimization studies on design and analysis of different type of steel truss stadium such as sub divided truss, Continuous truss and Arch truss can be carried out.
2. Combination of Steel truss Roof with Shell roof covering can be carried out for the stadiums such as Cricket Stadium, Rugby Stadium etc

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